September 1998

LM2679 SIMPLE

SWITCHER

® 5A

Step-Down

 Voltage Regulator

 with

Adjustable

 Current Limit

\int National Semiconductor

LM2679 SIMPLE SWITCHER® 5A Step-Down Voltage Regulator with Adjustable Current Limit

General Description

The LM2679 series of regulators are monolithic integrated circuits which provide all of the active functions for a step-down (buck) switching regulator capable of driving up to 5A loads with excellent line and load regulation characteristics. High efficiency (>90%) is obtained through the use of a low ON-resistance DMOS power switch. The series consists of fixed output voltages of 3.3V, 5V and 12V and an adjustable output version.

The SIMPLE SWITCHER® concept provides for a complete design using a minimum number of external components. A high fixed frequency oscillator (260KHz) allows the use of physically smaller sized components. A family of standard inductors for use with the LM2679 are available from several manufacturers to greatly simplify the design process.

Other features include the ability to reduce the input surge current at power-ON by adding a softstart timing capacitor to gradually turn on the regulator. The LM2679 series also has built in thermal shutdown and resistor programmable current limit of the power MOSFET switch to protect the device and load circuitry under fault conditions. The output voltage is guaranteed to a ±2% tolerance. The clock frequency is controlled to within a ±11% tolerance.

Features

- Efficiency up to 92%
- Simple and easy to design with (using off-the-shelf external components)
- Resistor programmable peak current limit over a range of 3A to 7A.
- $120 mΩ DMOS output switch$
- 3.3V, 5V and 12V fixed output and adjustable (1.2V to 37V) versions
- ±2%maximum output tolerance over full line and load conditions
- Wide input voltage range: 8V to 40V
- 260 KHz fixed frequency internal oscillator
- Softstart capability
- -40 to +125°C operating junction temperature range

Applications

- Simple to design, high efficiency (>90%) step-down switching regulators
- Efficient system pre-regulator for linear voltage regulators
- Battery chargers

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Absolute Maximum Ratings (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Operating Ratings

Electrical Characteristics Limits appearing in **bold type face** apply over the entire junction temperature range of operation, -40℃ to 125℃. Specifications appearing in normal type apply for $T_A = T_J = 25$ °C. $R_{ADJ} = 5.6$ KΩ

LM2679-3.3

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 \mathcal{L}^{max}

LM2679-5.0

LM2679-12

LM2679-ADJ

All Output Voltage Versions Electrical Characteristics

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Limits appearing in **bold type face** apply over the entire junction temperature range of operation, –40˚C to 125˚C.
Specifications appearing in normal type apply for T_A = T_J = 25˚C. Unless otherwise specified V_{IN}=12V

Note 1: Absolute Maximum Ratings are limits beyond which damage to the device may occur. Operating Ratings indicate conditions under which of the device is
guaranteed. Operating Ratings do not imply guaranteed performance acteristics tables.

Note 2: ESD was applied using the human-body model, a 100pF capacitor discharged through a 1.5 kΩ resistor into each pin.

Note 3: Typical values are determined with $T_A = T_J = 25^\circ \text{C}$ and represent the most likely norm.

Note 4: All limits are guaranteed at room temperature (standard type face) and at **temperature extremes (bold type face)**. All room temperature limits are 100% tested during production with T_A = T_J = 25°C. All limits at temperature extremes are guaranteed via correlation using standard standard Quality Control (SQC) meth-
ods. All limits are used to calculate Average Outgoing

Note 5: The peak switch current limit is determined by the following relationship: I_{CL}=37,125/ R_{ADJ}.

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Application Hints

The LM2679 provides all of the active functions required for a step-down (buck) switching regulator. The internal power switch is a DMOS power MOSFET to provide power supply designs with high current capability, up to 5A, and highly efficient operation.

The LM2679 is part of the **SIMPLE SWITCHER®** family of power converters. A complete design uses a minimum number of external components, which have been pre-determined from a variety of manufacturers. Using either this data sheet or a design software program called **LM267X Made Simple** (version 2.0) a complete switching power supply can be designed quickly. The software is provided free of charge and can be downloaded from National Semiconductor's Internet site located at http://www.national.com.

PIN 1 - Switch Output

This is the output of a power MOSFET switch connected directly to the input voltage. The switch provides energy to an inductor, an output capacitor and the load circuitry under control of an internal pulse-width-modulator (PWM). The PWM controller is internally clocked by a fixed 260KHz oscillator. In a standard step-down application the duty cycle (Time ON/Time OFF) of the power switch is proportional to the ratio of the power supply output voltage to the input voltage. The voltage on pin 1 switches between Vin (switch ON) and below ground by the voltage drop of the external Schottky diode (switch OFF).

PIN 2 - Input

The input voltage for the power supply is connected to pin 2. In addition to providing energy to the load the input voltage also provides bias for the internal circuitry of the LM2679. For guaranteed performance the input voltage must be in the range of 8V to 40V. For best performance of the power supply the input pin should always be bypassed with an input capacitor located close to pin 2.

PIN 3 - C Boost

A capacitor must be connected from pin 3 to the switch output, pin 1. This capacitor boosts the gate drive to the internal MOSFET above Vin to fully turn it ON. This minimizes con-

DESIGN CONSIDERATIONS

duction losses in the power switch to maintain high efficiency. The recommended value for C Boost is 0.01µF.

PIN 4 - Ground

This is the ground reference connection for all components in the power supply. In fast-switching, high-current applications such as those implemented with the LM2679, it is recommended that a broad ground plane be used to minimize signal coupling throughout the circuit

PIN 5 - Current Adjust

A key feature of the LM2679 is the ability to tailor the peak switch current limit to a level required by a particular application. This alleviates the need to use external components that must be physically sized to accommodate current levels (under shorted output conditions for example) that may be much higher than the normal circuit operating current requirements.

A resistor connected from pin 5 to ground establishes a current ($I_{\text{(pin 5)}}$ = 1.2V / R_{ADJ}) that sets the peak current through the power switch. The maximum switch current is fixed at a level of $37,125 / R_{ADJ}$.

PIN 6 - Feedback

This is the input to a two-stage high gain amplifier, which drives the PWM controller. It is necessary to connect pin 6 to the actual output of the power supply to set the dc output voltage. For the fixed output devices (3.3V, 5V and 12V outputs), a direct wire connection to the output is all that is required as internal gain setting resistors are provided inside the LM2679. For the adjustable output version two external resistors are required to set the dc output voltage. For stable operation of the power supply it is important to prevent coupling of any inductor flux to the feedback input.

PIN 7 - Softstart

A capacitor connected from pin 7 to ground allows for a slow turn-on of the switching regulator. The capacitor sets a time delay to gradually increase the duty cycle of the internal power switch. This can significantly reduce the amount of surge current required from the input supply during an abrupt application of the input voltage. If softstart is not required this pin should be left open circuited.

Power supply design using the LM2679 is greatly simplified by using recommended external components. A wide range of inductors, capacitors and Schottky diodes from several manufacturers have been evaluated for use in designs that cover the full range of capabilities (input voltage, output voltage and load current) of the LM2679. A simple design procedure using nomographs and component tables provided in this data sheet leads to a working design with very little effort. Alternatively, the design software, **LM267X Made Simple** (version 2.0), can also be used to provide instant component selection, circuit performance calculations for evaluation, a bill of materials component list and a circuit schematic.

The individual components from the various manufacturers called out for use are still just a small sample of the vast array of components available in the industry. While these components are recommended, they are not exclusively the only components for use in a design. After a close comparison of component specifications, equivalent devices from other manufacturers could be substituted for use in an application.

Important considerations for each external component and an explanation of how the nomographs and selection tables were developed follows.

INDUCTOR

The inductor is the key component in a switching regulator. For efficiency the inductor stores energy during the switch ON time and then transfers energy to the load while the switch is OFF.

Nomographs are used to select the inductance value required for a given set of operating conditions. The nomographs assume that the circuit is operating in continuous mode (the current flowing through the inductor never falls to zero). The magnitude of inductance is selected to maintain a maximum ripple current of 30% of the maximum load current. If the ripple current exceeds this 30% limit the next larger value is selected.

The inductors offered have been specifically manufactured to provide proper operation under all operating conditions of input and output voltage and load current. Several part types are offered for a given amount of inductance. Both surface mount and through-hole devices are available. The inductors from each of the three manufacturers have unique characteristics.

Renco: ferrite stick core inductors; benefits are typically lowest cost and can withstand ripple and transient peak currents above the rated value. These inductors have an external magnetic field, which may generate EMI.

Pulse Engineering: powdered iron toroid core inductors; these also can withstand higher than rated currents and, being toroid inductors, will have low EMI.

Coilcraft: ferrite drum core inductors; these are the smallest physical size inductors and are available only as surface mount components. These inductors also generate EMI but less than stick inductors.

OUTPUT CAPACITOR

The output capacitor acts to smooth the dc output voltage and also provides energy storage. Selection of an output capacitor, with an associated equivalent series resistance (ESR), impacts both the amount of output ripple voltage and stability of the control loop.

The output ripple voltage of the power supply is the product of the capacitor ESR and the inductor ripple current. The capacitor types recommended in the tables were selected for having low ESR ratings.

In addition, both surface mount tantalum capacitors and through-hole aluminum electrolytic capacitors are offered as solutions.

Impacting frequency stability of the overall control loop, the output capacitance, in conjunction with the inductor, creates a double pole inside the feedback loop. In addition the capacitance and the ESR value create a zero. These frequency response effects together with the internal frequency compensation circuitry of the LM2679 modify the gain and phase shift of the closed loop system.

As a general rule for stable switching regulator circuits it is desired to have the unity gain bandwidth of the circuit to be limited to no more than one-sixth of the controller switching frequency. With the fixed 260KHz switching frequency of the LM2679, the output capacitor is selected to provide a unity gain bandwidth of 40KHz maximum. Each recommended capacitor value has been chosen to achieve this result.

In some cases multiple capacitors are required either to reduce the ESR of the output capacitor, to minimize output ripple (a ripple voltage of 1% of Vout or less is the assumed performance condition), or to increase the output capacitance to reduce the closed loop unity gain bandwidth (to less than 40KHz). When parallel combinations of capacitors are required it has been assumed that each capacitor is the exact same part type.

The RMS current and working voltage (WV) ratings of the output capacitor are also important considerations. In a typical step-down switching regulator, the inductor ripple current (set to be no more than 30% of the maximum load current by the inductor selection) is the current that flows through the output capacitor. The capacitor RMS current rating must be greater than this ripple current. The voltage rating of the output capacitor should be greater than 1.3 times the maximum output voltage of the power supply. If operation of the system at elevated temperatures is required, the capacitor voltage rating may be de-rated to less than the nominal room temperature rating. Careful inspection of the manufacturer's specification for de-rating of working voltage with temperature is important.

INPUT CAPACITOR

Fast changing currents in high current switching regulators place a significant dynamic load on the unregulated power source. An input capacitor helps to provide additional current to the power supply as well as smooth out input voltage variations.

Like the output capacitor, the key specifications for the input capacitor are RMS current rating and working voltage. The RMS current flowing through the input capacitor is equal to one-half of the maximum dc load current so the capacitor should be rated to handle this. Paralleling multiple capacitors proportionally increases the current rating of the total capacitance. The voltage rating should also be selected to be 1.3 times the maximum input voltage. Depending on the unregulated input power source, under light load conditions the maximum input voltage could be significantly higher than normal operation and should be considered when selecting an input capacitor.

The input capacitor should be placed very close to the input pin of the LM2679. Due to relative high current operation with fast transient changes, the series inductance of input connecting wires or PCB traces can create ringing signals at the input terminal which could possibly propagate to the output or other parts of the circuitry. It may be necessary in some designs to add a small valued (0.1µF to 0.47µF) ceramic type capacitor in parallel with the input capacitor to prevent or minimize any ringing.

CATCH DIODE

When the power switch in the LM2679 turns OFF, the current through the inductor continues to flow. The path for this current is through the diode connected between the switch output and ground. This forward biased diode clamps the switch output to a voltage less than ground. This negative voltage must be greater than −1V so a low voltage drop (particularly at high current levels) Schottky diode is recommended. Total efficiency of the entire power supply is significantly impacted by the power lost in the output catch diode. The average current through the catch diode is dependent on the switch duty cycle (D) and is equal to the load current times (1-D). Use of a diode rated for much higher current than is required by the actual application helps to minimize the voltage drop and power loss in the diode.

During the switch ON time the diode will be reversed biased by the input voltage. The reverse voltage rating of the diode should be at least 1.3 times greater than the maximum input voltage.

BOOST CAPACITOR

The boost capacitor creates a voltage used to overdrive the gate of the internal power MOSFET. This improves efficiency by minimizing the on resistance of the switch and associated power loss. For all applications it is recommended to use a 0.01µF/50V ceramic capacitor.

RADJ, ADJUSTABLE CURRENT LIMIT

A key feature of the LM2679 is the ability to control the peak switch current. Without this feature the peak switch current would be internally set to 7A or higher to accommodate 5A load current designs. This requires that both the inductor (which could saturate with excessively high currents) and the catch diode be able to safely handle up to 7A which would be conducted under load fault conditions.

If an application only requires a load current of 3A or 4A the peak switch current can be set to a limit just over the maximum load current with the addition of a single programming resistor. This allows the use of less powerful and more cost effective inductors and diodes.

The peak switch current is equal to a factor of 37,125 divided by R_{ADJ}. A resistance of 5.6K Ω sets the current limit to typically 6.3A and an R_{ADJ} of 8.25K Ω reduces the maximum current to approximately 4.4A. For predictable control of the current limit it is recommended to keep the peak switch current greater than 3A. For lower current applications a 3A switching regulator with adjustable current limit, the LM2673, is available.

When the power switch reaches the current limit threshold it is immediately turned OFF and the internal switching frequency is reduced. This extends the OFF time of the switch to prevent a steady state high current condition. As the switch current falls below the current limit threshold, the switch will turn back ON. If a load fault continues, the switch will again exceed the threshold and switch back OFF. This will result in a low duty cycle pulsing of the power switch to minimize the overall fault condition power dissipation.

Css SOFTSTART CAPACITOR

This optional capacitor controls the rate at which the LM2679 starts up at power on. The capacitor is charged linearly by an internal current source. This voltage ramp gradually increases the duty cycle of the power switch until it reaches the normal operating duty cycle defined primarily by the ratio of the output voltage to the input voltage. The softstart turn-on time is programmable by the selection of Css. The formula for selecting a softstart capacitor is:

$$
C_{SS} \cong (I_{SST} \cdot t_{SS}) / [V_{SST} + 2.6V \cdot (\frac{V_{OUT} + V_{SCHOTTKY}}{V_{IN}})]
$$

Where:

 I_{SST} = Softstart Current, 3.7 μ A typical

 t_{SS} = Softstart time, from design requirements

 V_{SST} = Softstart Threshold Voltage, 0.63V typical

 V_{OUT} = Output Voltage, from design requirements V_{SCHOTTKY} = Schottky Diode Voltage Drop, typically 0.5V V_{IN} = Maximum Input Voltage, from design requirements

If this feature is not desired, leave the Softstart pin (pin 7) open circuited

SIMPLE DESIGN PROCEDURE

Using the nomographs and tables in this data sheet (or use the available design software at http://www.national.com) a complete step-down regulator can be designed in a few simple steps.

Step 1: Define the power supply operating conditions:

Required output voltage

Maximum DC input voltage

Maximum output load current

Step 2: Set the output voltage by selecting a fixed output LM2679 (3.3V, 5V or 12V applications) or determine the required feedback resistors for use with the adjustable LM2679−ADJ

Step 3: Determine the inductor required by using one of the four nomographs, Figure 3 through Figure 6. Table 1 provides a specific manufacturer and part number for the inductor.

Step 4: Using Table 3 (fixed output voltage) or Table 6 (adjustable output voltage), determine the output capacitance required for stable operation. Table 2 provides the specific capacitor type from the manufacturer of choice.

Step 5: Determine an input capacitor from Table 4 for fixed output voltage applications. Use Table 2 to find the specific capacitor type. For adjustable output circuits select a capacitor from Table 2 with a sufficient working voltage (WV) rating greater than Vin max, and an rms current rating greater than one-half the maximum load current (2 or more capacitors in parallel may be required).

Step 6: Select a diode from Table 5. The current rating of the diode must be greater than I load max and the Reverse Voltage rating must be greater than Vin max.

Step 7: Include a 0.01µF/50V capacitor for Cboost in the design and then determine the value of a softstart capacitor if desired.

Step 8: Define a value for R_{ADJ} to set the peak switch current limit to be at least 20% greater than Iout max to allow for at least 30% inductor ripple current (±15% of Iout). For designs that must operate over the full temperature range the switch current limit should be set to at least 50% greater than lout max (1.5 x I_{out} max).

FIXED OUTPUT VOLTAGE DESIGN EXAMPLE

A system logic power supply bus of 3.3V is to be generated from a wall adapter which provides an unregulated DC voltage of 13V to 16V. The maximum load current is 4A. A softstart delay time of 50mS is desired. Through-hole components are preferred.

Step 1: Operating conditions are:

Vout = $3.3V$

Vin max = $16V$

Iload max = 4A

Step 2: Select an LM2679T-3.3. The output voltage will have a tolerance of

±2% at room temperature and ±3% over the full operating temperature range.

Step 3: Use the nomograph for the 3.3V device , Figure 3. The intersection of the 16V horizontal line (V_{in} max) and the 4A vertical line (I_{load} max) indicates that L46, a 15 μ H inductor, is required.

From Table 1, L46 in a through-hole component is available from Renco with part number RL-1283-15-43.

Step 4: Use Table 3 to determine an output capacitor. With a 3.3V output and a 15µH inductor there are four through-hole output capacitor solutions with the number of same type capacitors to be paralleled and an identifying capacitor code given. Table 2 provides the actual capacitor characteristics. Any of the following choices will work in the circuit:

2 x 220µF/10V Sanyo OS-CON (code C5)

2 x 820µF/16V Sanyo MV-GX (code C5)

- 1 x 3900µF/10V Nichicon PL (code C7)
- 2 x 560µF/35V Panasonic HFQ (code C5)

Step 5: Use Table 4 to select an input capacitor. With 3.3V output and 15µH there are three through-hole solutions. These capacitors provide a sufficient voltage rating and an rms current rating greater than $2A (1/2 I_{load}$ max). Again using Table 2 for specific component characteristics the following choices are suitable:

2 x 680µF/63V Sanyo MV-GX (code C13)

1 x 1200µF/63V Nichicon PL (code C25)

1 x 1500µF/63V Panasonic HFQ (code C16)

Step 6: From Table 5 a 5A or more Schottky diode must be selected. For through-hole components only 40V rated diodes are indicated and 4 part types are suitable:

1N5825

MBR745

80SQ045

6TQ045

Step 7: A 0.01µF capacitor will be used for Cboost. For the 50mS softstart delay the following parameters are to be used:

 $I_{SST}: 3.7 μ A$

 t_{SS} : 50mS

 V_{SST} : 0.63V

 V_{OUT} : 3.3V

V_{SCHOTTKY}: 0.5V V_{IN} : 16V

Using Vin max ensures that the softstart delay time will be at least the desired 50mS.

Using the formula for Css a value of 0.148µF is determined to be required. Use of a standard value 0.22µF capacitor will produce more than sufficient softstart delay.

Step 8: Determine a value for R_{ADJ} to provide a peak switch current limit of at least 4A plus 50% or 6A.

$$
R_{\text{ADJ}} = \frac{37,125}{6\text{A}} = 6.1875 \text{ k}\Omega
$$

Use a value of 6.2KΩ.

ADJUSTABLE OUTPUT DESIGN EXAMPLE

In this example it is desired to convert the voltage from a two battery automotive power supply (voltage range of 20V to 28V, typical in large truck applications) to the 14.8VDC alternator supply typically used to power electronic equipment from single battery 12V vehicle systems. The load current required is 3.5A maximum. It is also desired to implement the power supply with all surface mount components. Softstart is not required.

Step 1: Operating conditions are:

Vout = $14.8V$ Vin max $= 28V$ $Iload$ max = 3.5A

Step 2: Select an LM2679S-ADJ. To set the output voltage to 14.9V two resistors need to be chosen (R1 and R2 in Figure 2). For the adjustable device the output voltage is set by the following relationship:

$$
V_{\text{OUT}} = V_{FB} \left(1 + \frac{R_2}{R_1} \right)
$$

Where V_{FB} is the feedback voltage of typically 1.21V. A recommended value to use for R1 is 1K. In this example then R2 is determined to be:

$$
R_2 = R_1 \left(\frac{V_{\text{OUT}}}{V_{\text{FB}}} - 1 \right) = 1 k \Omega \left(\frac{14.8 V}{1.21 V} - 1 \right)
$$

R2 = 11.23KΩ

The closest standard 1% tolerance value to use is 11.3KΩ This will set the nominal output voltage to 14.88V which is within 0.5% of the target value.

Step 3: To use the nomograph for the adjustable device, Figure 6, requires a calculation of the inductor Volt•microsecond constant (E•T expressed in V•µS) from the following formula: \sim 100

$$
E \cdot T = (V_{IN(MAX)} - V_{OUT} - V_{SAT}) \cdot \frac{V_{OUT} + V_D}{V_{IN(MAX)} - V_{SAT} + V_D} \cdot \frac{1000}{260} (V \cdot \mu s)
$$

where V_{SAT} is the voltage drop across the internal power switch which is $R_{ds(ON)}$ times I_{load} . In this example this would be typically 0.12Ω x 3.5A or 0.42V and V_D is the voltage drop across the forward bisased Schottky diode, typically 0.5V. The switching frequency of 260KHz is the nominal value to use to estimate the ON time of the switch during which energy is stored in the inductor. For this example E•T is found to be:

$$
E \cdot T = (28 - 14.8 - 0.42) \cdot \frac{14.8 + 0.5}{28 - 0.42 + 0.5} \cdot \frac{1000}{260} \text{ (V} \cdot \mu\text{s})
$$

$$
E \cdot T = (12.78 \text{V}) \cdot \frac{15.3 \text{V}}{28.08 \text{V}} \cdot 3.85 \text{ (V} \cdot \mu\text{s}) = 26.8 \text{ (V} \cdot \mu\text{s})
$$

Using Figure ⁶, the intersection of 27V•µS horizontally and the 3.5A vertical line (I_{load} max) indicates that L48, a 47 μ H inductor, or L49, a 33µH inductor could be used. Either inductor will be suitable, but for this example selecting the larger inductance will result in lower ripple current.

From Table 1, L48 in a surface mount component is available from Pulse Engineering with part number P0848.

Step 4: Use Table 6 to determine an output capacitor. With a 14.8V output the 12.5 to 15V row is used and with a 47µH inductor there are three surface mount output capacitor solutions. Table 2 provides the actual capacitor characteristics based on the C Code number. Any of the following choices can be used:

- 1 x 33µF/20V AVX TPS (code C6)
- 1 x 47µF/20V Sprague 594 (code C8)
- 1 x 47µF/20V Kemet T495 (code C8)

Important Note: When using the adjustable device in low voltage applications (less than 3V output), if the nomograph, Figure 6, selects an inductance of 22µH or less, Table 6 does not provide an output capacitor solution. With these conditions the number of output capacitors required for stable operation becomes impractical. It is recommended to use either a 33µH or 47µH inductor and the output capacitors from Table 6.

Step 5: An input capacitor for this example will require at least a 35V WV rating with an rms current rating of 1.75A (1/2 Iout max). From Table 2 it can be seen that C12, a 33µF/35V capacitor from Sprague, has the highest voltage/current rating of the surface mount components and that two of these capacitor in parallel will be adquate.

Step 6: From Table 5 a 5A or more Schottky diode must be selected. For surface mount diodes with a margin of safety on the voltage rating one of two diodes can be used: MBRD1545CT

6TQ045S

Step 7: A 0.01µF capacitor will be used for Cboost.

The softstart pin will be left open circuited.

Step 8: Determine a value for R_{ADJ} to provide a peak switch current limit of at least 3.5A plus 50% or 5.25A.

$$
R_{\text{ADJ}} = \frac{37,125}{5.24} = 7.14 \text{ k}.
$$

Use a value of 7.15KΩ.

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Table 1. Inductor Manufacturer Part Numbers

Inductor Manufacturer Contact Numbers

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Table 2. Input and Output Capacitor Codes

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Table 2. Input and Output Capacitor Codes (continued)

Capacitor Manufacturer Contact Numbers

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Table 3. Output Capacitors for Fixed Output Voltage Application

No. represents the number of identical capacitor types to be connected in parallel C Code indicates the Capacitor Reference number in Table 2 for identifying the specific component from the manufacturer.

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Table 4. Input Capacitors for Fixed Output Voltage Application

(Assumes worst case maximum input voltage and load current for a given inductance value)

* Check voltage rating of capacitors to be greater than application input voltage.
No. represents the number of identical capacitor types to be connected in parallel
C Code indicates the Capacitor Reference number in Table

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Table 5. Schottky Diode Selection Table

Diode Manufacturer Contact Numbers

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Table 6. Output Capacitors for Adjustable Output Voltage Applications

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Table 6. Output Capacitors for Adjustable Output Voltage Applications (continued)

* Set to a higher value for a practical design solution. See Applications Hints section
No. represents the number of identical capacitor types to be connected in parallel
C Code indicates the Capacitor Reference number in

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